

Gas Solubilities, Vapor-Liquid Equilibria, and Partial Molal Volumes in Some Hydrogen-Hydrocarbon Systems

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Gas solubilities were measured for hydrogen in *n*-pentane, 2,3-dimethylbutane, cyclohexane, *n*-decane, *m*-xylene, 1,4-diehybenzene, and 1-methylnaphthalene.

Vapor-liquid equilibrium ratios (*K*'s) were measured for the second, third, fifth, and sixth of these systems. Partial molal volumes of hydrogen dissolved in the liquid hydrocarbons were measured for all systems except methylnaphthalene. Temperatures and pressures fell in the ranges 35-320 °C and 200-2400 psi.

Introduction

Because hydrogen is used in petroleum processing, physical properties of hydrogen-hydrocarbon systems are often necessary for the design of refinery units. This paper adds to the previous data (1, 2) which we have reported on such systems. Gas solubilities for seven systems, vapor-liquid equilibrium ratios for four systems, and partial molal volumes for six systems are reported here.

Experimental Section

The hydrocarbons used were American Petroleum Institute standard samples with stated purities of 99.9+ mol %. The experimental method has been described in detail (1). Briefly, a small sample of known mass and composition was confined above mercury in a glass capillary. Then, as the liquid mixture was expanded at constant temperature, the pressures at which the first trace of gas appeared (bubble-point pressure) and the last trace of liquid disappeared (dew-point pressure) were measured. The bubble-point pressures yield gas solubilities, and in a two-component system the combination of bubble- and dew-point pressures yields the vapor-liquid equilibrium ratios (*K*'s) for the system.

Partial molal volumes were derived by measuring the expansion which occurs when hydrogen is mixed with liquid hydrocarbon in a glass capillary (3).

The temperature can be set from 35 to 370 °C, but it was usually kept below 300 °C to avoid thermal decomposition. Pressure can be set from 100 to 3000 psi, but it was usually kept below 2500 psi to avoid frequent capillary replacement.

Gas Solubilities

Because gas solubilities are fairly linear with "partial pressure", the bubble points can be represented by equations of the form

$$S = a + b(p - p_1^0) + c(p - p_1^0)^2 \quad (1)$$

where *a*, *b*, and *c* are constants at each temperature and are given in Table I; *S* is a "solubility" defined by $S = (x_2/x_1)/(p - p_1^0)$; *x* is a mole fraction in the liquid; *p* is a bubble pressure, p_1^0 is a vapor pressure, and subscripts 1 and 2 denote hydrocarbon and hydrogen, respectively.

These definitions of "solubility" and "partial pressure" are, of course, only arbitrary devices to simplify the representation

of bubble pressure. As a definition of partial pressure, $p - x_1 p_1^0$ works somewhat better than $p - p_1^0$, but not enough better to warrant the added complexity in solving eq 1 for *x*₂ (given *p*). p_1^0 is an approximate vapor pressure which is calculated from Table II. Of course, this particular p_1^0 must always be used in conjunction with the constants in Table I.

The experimental bubble pressures, along with the deviations from eq 1, are listed in Table III.

Vapor-Liquid Equilibrium Ratios

Vapor-liquid equilibrium ratios, or *K*'s, are defined by

$$K_1 = y_1/x_1 \quad K_2 = y_2/x_2 \quad (2)$$

where *y* and *x* are mole fractions in the vapor and liquid, and subscripts 1 and 2 refer to hydrocarbon and hydrogen. For a binary system, *K* is a function of temperature and pressure only.

At each experimental dew point (listed under psi in Table IV) the vapor composition was known, and the corresponding liquid composition was calculated from eq 1. These compositions were then used to calculate the vapor-liquid equilibrium ratios listed in Table IV.

The function *pK*, where *p* is the pressure of the system, varies more slowly with pressure than does *K*. Therefore, interpolation to convenient values of pressure was accomplished by plotting *pK* as a function of pressure at constant temperature on large-scale graph paper. Reduced versions of these plots are shown in Figures 1-8.

Smoothed *K*'s, listed in Table V, were read from the *pK* plots. Those values in parentheses are dependent on short extensions of eq 1 (linear form only) to pressures higher than observed bubble pressures. Values of *K* for two other hydrogen-hydrocarbon systems have been reported (2).

Partial Molal Volumes

Partial molal volumes of gases in liquid solutions are necessary in the calculation of thermodynamic properties of solutions from liquid-vapor-equilibrium and gas-compressibility data at high pressures (1). Because the literature usually reports only room-temperature partial molal volumes for gas-hydrocarbon systems, and because our apparatus easily combines these measurements with bubble points, we have made numerous high-temperature partial-molal-volume measurements. The volume-expansion method used has been described (3).

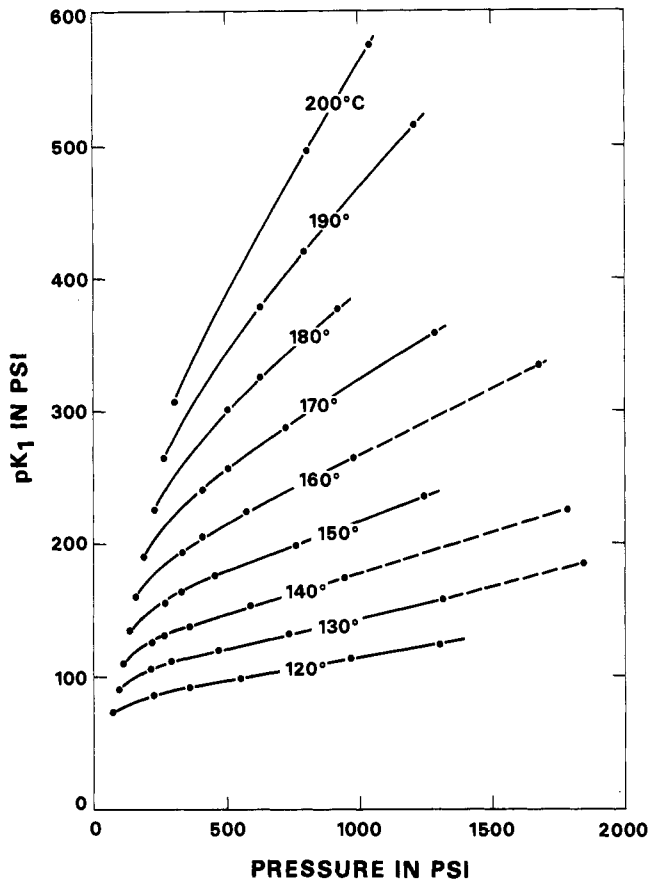
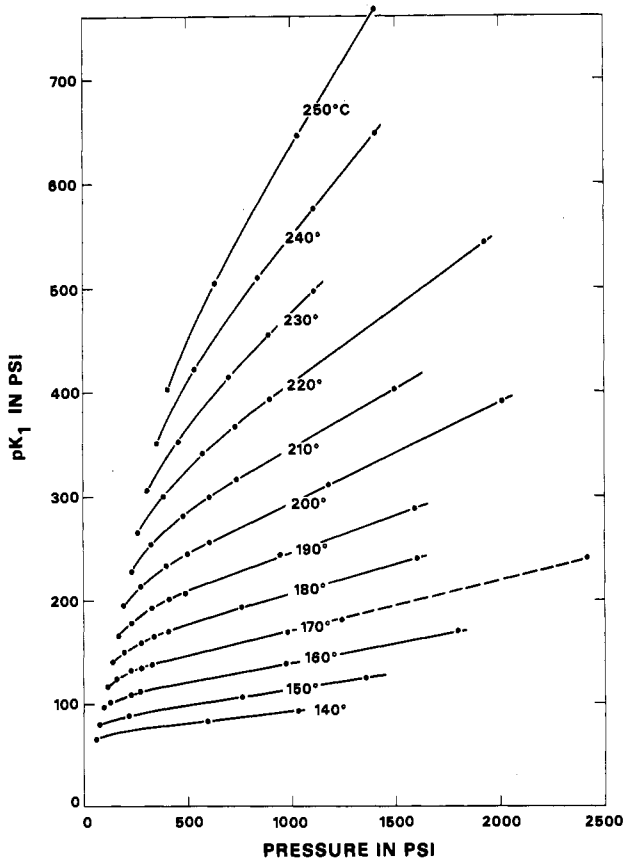
At gas concentration below 10 or 15 mol %, the volume expansion of liquid per mol of gas dissolved varies linearly with composition at constant temperature and pressure; i.e.

$$\Delta V/n_2 = \bar{V}_2^* + c'x_2 \quad (3)$$

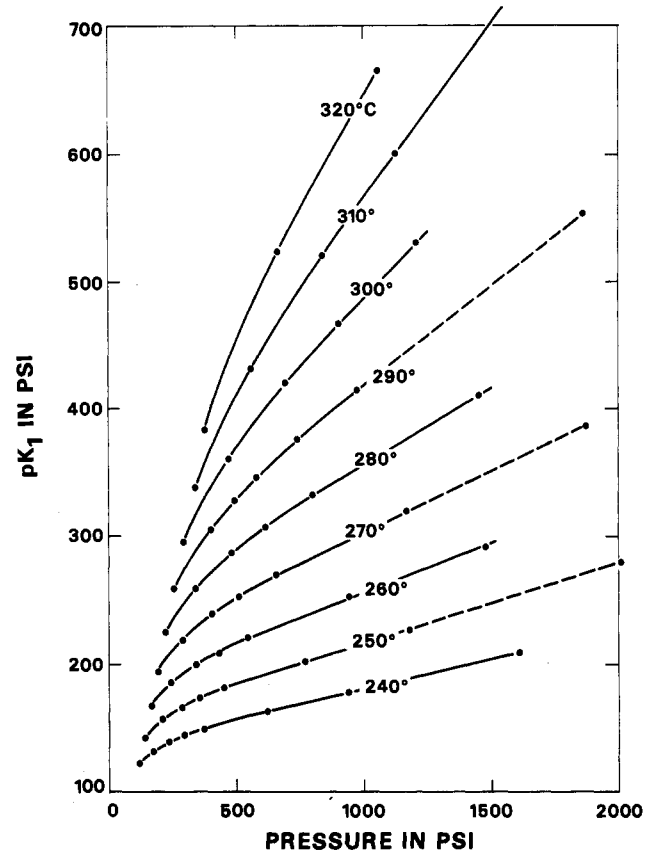
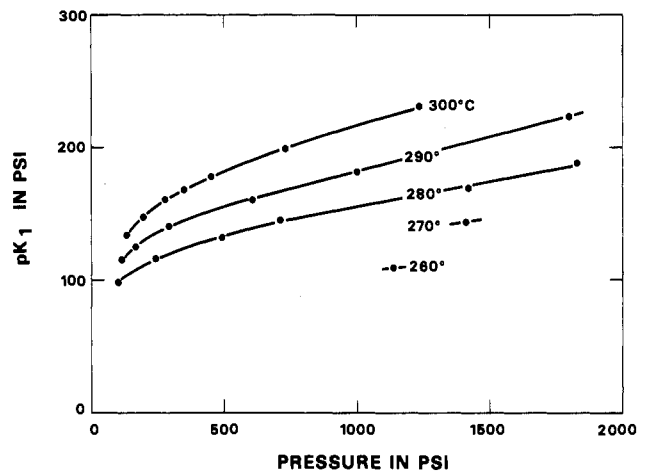
where ΔV is the measured volume expansion of the liquid when *n*₂ moles of gas are dissolved in pure hydrocarbon to give a mole fraction *x*₂, and \bar{V}_2^* is the gas partial molal volume at infinite dilution. \bar{V}_2^* and *c'* are functions of temperature and pressure only. That the intercept is \bar{V}_2^* follows from the definition

$$\bar{V}_2^* = \lim_{n_2 \rightarrow 0} (\Delta V/n_2)_{T,p,n_1}$$

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Figure 1. pK_1 for 2,3-dimethylbutane.Figure 2. pK_1 for cyclohexane.

Values of c' obtained from eq 3 are approximately related to the composition variation of partial molal volumes \bar{V}_1 and \bar{V}_2 :

Figure 3. pK_1 for *m*-xylene.Figure 4. pK_1 for 1,4-diethylbenzene.

i.e., assume that the molal volume of the solution, V , can be represented as a Taylor series in the mole fraction of hydrogen, x_2 , for small x_2 . Then

$$V = V_1 + b'x_2 + c'x_2^2 + \dots \quad (4)$$

where V_1 is the molal volume of the pure hydrocarbon, b' and c' are functions of temperature and pressure, and we neglect cubic and higher terms. By definition we have

$$\bar{V}_1 = (\partial nV / \partial n_1)_{T,p,n} \quad (5)$$

where $n = n_1 + n_2$ is the total number of moles in solution and V , the solution molal volume, is given by $V = x_1\bar{V}_1 + x_2\bar{V}_2$. Applying eq 5 to eq 4 we obtain

$$\bar{V}_1 - V_1 = -c'x_2^2 \quad (6)$$

$$\bar{V}_2 - \bar{V}_2^* = 2c'x_2 \quad (7)$$

Table I. Solubilities of Hydrogen in Hydrocarbons^a

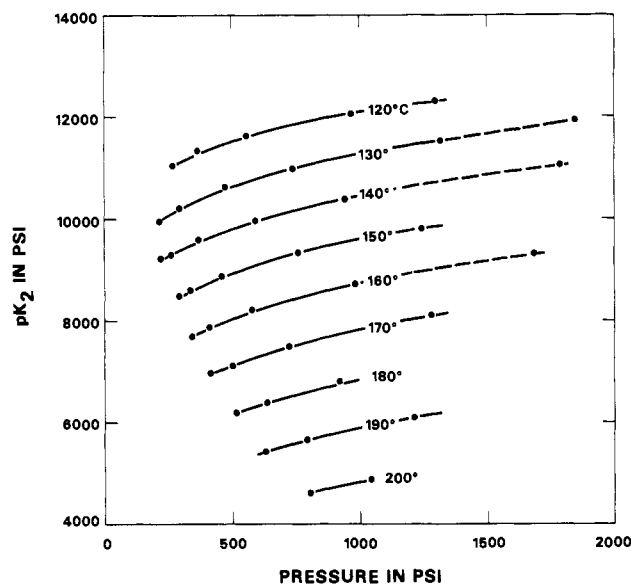
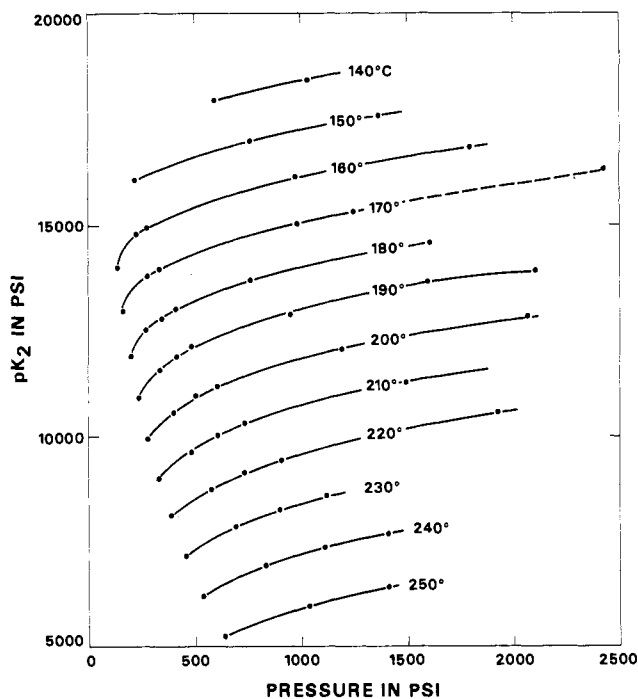
t°C	n-pentane		2,3-dimethylbutane		n-decane		cyclohexane		m-xylene		1,4-dimethylbenzene		1-methylisophtalene		
	ax10 ³ bx10 ⁵ cx10 ⁶	S.D.Z. DP,MP	ax10 ³ bx10 ⁵ cx10 ⁶	S.D.Z. DP,MP	ax10 ³ bx10 ⁵ cx10 ⁶	S.D.Z. DP,MP	ax10 ³ bx10 ⁵ cx10 ⁶	S.D.Z. DP,MP	ax10 ³ bx10 ⁵ cx10 ⁶	S.D.Z. DP,MP	ax10 ³ bx10 ⁵ cx10 ⁶	S.D.Z. DP,MP	ax10 ³ bx10 ⁵ cx10 ⁶	S.D.Z. DP,MP	
35	.7897	.0036	.14	4,20	.7751	.0004	.05	4,22	.7408	-.0110	.08	4,23			
40	.8142	.0053	.13	4,19	.7979	.0014	.09	4,21							
50	.8656	.0084	.17	4,17	.8440	.0043	.06	4,20							
60	.9196	.0129	.20	4,17	.8931	.0067	.08	5,23							
70	.9783	.0155	.15	5,20	.9435	.0110	.20	5,23	.8904	-.0073	.09	5,24	.5414	-.0014	
80	1.0389	.0235	.15	5,19	.9974	.0140	.09	5,21							
90	1.1037	.0300	.15	5,18	1.0533	.0196	.09	5,20	.6122	.0006	.06	3,20			
100	1.1774	.0399	.15	5,17	1.1131	.0251	.08	5,19	.6497	.0017	.08	3,19			
110	1.2573	.0506	.17	5,16	1.1772	.0323	.10	5,18	1.0799	-.0031	.11	6,23	.6885	.0034	
120	1.3452	.0600	.18	5,15	1.2456	.0398	.30	5,17	.7284	.0056	.08	4,23			
130	1.4481	.0779	.20	5,15	1.3223	.0469	.14	5,16	.7734	.0076	.07	4,21			
140	1.5614	.1120	.21	5,14	1.4059	.0624	.11	5,15	1.2375	.0021	.11	6,20	.8153	.0105	
150	1.7011	.1466	.24	5,13	1.4987	.0788	.12	5,14	.8621	.0146	.04	4,19			
160	1.8721	.2035	.31	5,12	1.6042	.1001	.13	5,14	1.3524	.0082	.12	6,18	.9125	.0187	
170	2.0911	.3114	.39	5,12	1.7254	.1304	.14	5,13	.9661	.0242	.03	5,23			
180	2.4108	.4620	.0184	.42	5,11	1.8702	.1727	.19	5,13	1.4775	.0176	.17	6,17	1.0261	.0297
190	2.9667	.9951	.2000	.43	5,9	2.0471	.2409	.22	5,12	1.0905	.0370	.07	5,20		
200						2.2762	.3639	.18	5,11	1.6207	.0238	.15	6,15	1.1627	.0461
210						2.5938	.6568	.44	5,11	1.2831	.0575	.13	6,19		
220										1.7832	.0362	.14	6,14		
230										1.4471	.0937	.22	5,17		
240										1.9728	.0529	.14	6,13	1.5789	.1273
250										2.0820	.0636	.16	6,12	1.7573	.1266
260										2.2043	.0747	.15	6,11		
270										2.3442	.0864	.30	6,11		
280										2.5159	.0228	.0106	.25	6,11	
290										2.7128	-.0112	.0182	.23	6,10	
300										2.9169	.1295	.0078	.20	6,10	
310										1.8844	.0469	.08	5,14		
320										2.1172	.0449	.49	5,13		

^aSolubility = $S = (x_2/x_1)/(p - p_1^0)$. $S = a + b(p - p_1^0) + c(p - p_1^0)^2$. DP,MP = number of data points, maximum pressure of measurements in hundreds of psi. p is pressure in (lb/in.²)/14.696, p_1^0 is a vapor pressure (Table II).

Table II. Vapor Pressure Constants^a (4)

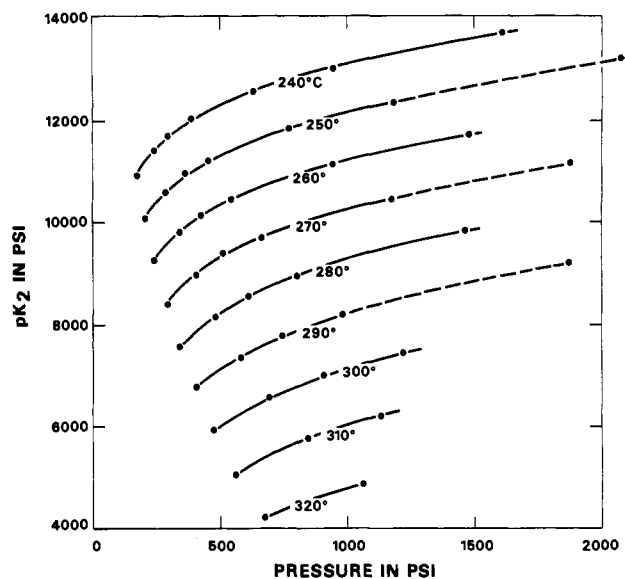
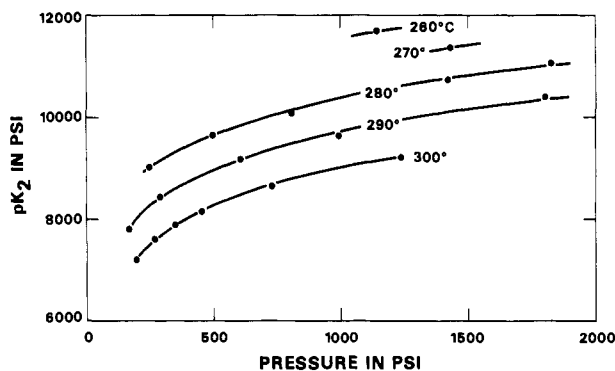
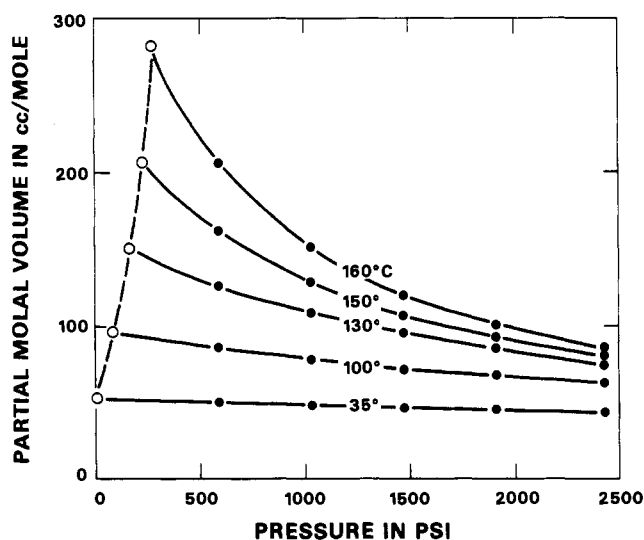
	A	B	C	T _c , K
<i>n</i> -pentane	6.852 21	1064.630	232.000	470
2,3-dimethylbutane	6.809 83	1127.187	228.900	500
cyclohexane	6.844 98	1203.526	222.863	554
<i>n</i> -decane	6.953 67	1501.268	194.480	619
<i>m</i> -xylene	7.009 08	1462.266	215.105	619
1,4-diethylbenzene	7.000 54	1589.273	202.019	662
1-methylnaphthalene	7.068 99	1852.674	192.716	787

^a $\log(760 p_1^0) = A - B/(T + C) + 0.50(T/T_c - 0.75)^2$. Omit last term when $T/T_c < 0.75$. p_1^0 is vapor pressure in (lb/in.²)/14.696.

Figure 5. pK_2 for 2,3-dimethylbutane.Figure 6. pK_2 for cyclohexane.

and if we use $\Delta V = nV - n_1V_1$, the c' in eq 6 and 7 can be identified with c' of eq 3. It turns out that $c' > 0$ so that \bar{V}_1 decreases slowly as H_2 is added and \bar{V}_2 increases fairly rapidly. The liquid-phase activity coefficients show this same asymmetry in behavior (1).

Experimental values for the solution dilation $\Delta V/n_2$, are available as supplementary material. Because there are sev-

Figure 7. pK_2 for *m*-xylene.Figure 8. pK_2 for 1,4-diethylbenzene.Figure 9. Partial molal volumes of hydrogen, at infinite dilution, in liquid *n*-pentane.

eral thousand of these values, and because we wish to derive partial molal volumes, an analytical representation is desirable. Previous work (1) has shown that the reciprocals of the dilute solution partial molal volumes, \bar{V}_2^* , are linear with pressure up to about 1600 psi. A small quadratic term is sufficient to take care of any curvature between 1600 and 2500 psi. The

Table III. Measured Solubilities of Hydrogen in Hydrocarbons

°C	psi	x ₂	Δx	°C	psi	x ₂	Δx	°C	psi	x ₂	Δx	°C	psi	x ₂	Δx
n-PENTANE															
35.00	508.8	0.07592	-0.01	120.00	355.5	0.02679	0.15	90.00	504.5	0.01982	0.05	230.00	509.6	0.01987	0.16
35.00	1037.2	0.05231	-0.23	120.00	673.6	0.04901	0.02	90.00	1111.0	0.04349	-0.08	230.00	759.6	0.04349	-0.12
35.00	1528.4	0.07542	0.21	120.00	1048.9	0.07759	-0.06	90.00	2051.9	0.07817	0.02	230.00	1138.3	0.07817	-0.14
35.00	1975.8	0.09596	0.10	120.00	1415.5	0.10488	0.09	100.00	482.2	0.01982	0.06	230.00	1385.9	0.10019	-0.00
40.00	478.1	0.02592	0.01	120.00	1732.7	0.12728	0.10	100.00	1053.1	0.04349	0.10	230.00	1732.4	0.12996	0.09
40.00	966.2	0.05231	0.08	130.00	394.0	0.02679	0.09	100.00	1936.2	0.07817	0.05	240.00	538.1	0.01982	0.16
40.00	1452.7	0.07542	-0.27	130.00	568.5	0.04901	-0.15	110.00	4033.7	0.01982	0.05	240.00	766.5	0.04349	-0.14
40.00	1942.7	0.09596	-0.20	130.00	1004.8	0.07759	-0.05	110.00	1060.7	0.04349	-0.05	240.00	1111.2	0.07817	-0.14
40.00	2432.7	0.11975	0.10	130.00	1354.1	0.10488	0.01	110.00	1832.7	0.07817	0.01	240.00	1334.9	0.10019	0.06
50.00	454.7	0.02592	0.02	140.00	395.8	0.02679	0.09	120.00	548.4	0.01982	0.09	250.00	1649.2	0.12996	0.07
50.00	933.8	0.05231	0.08	140.00	641.3	0.04901	-0.10	120.00	955.7	0.04349	0.09	250.00	565.9	0.01931	0.10
50.00	1393.8	0.07542	-0.23	140.00	967.0	0.07759	-0.08	120.00	1738.5	0.07817	-0.09	250.00	570.5	0.01982	-0.08
50.00	1892.1	0.09596	-0.13	140.00	1293.2	0.10488	-0.01	120.00	2261.0	0.10019	-0.07	250.00	775.8	0.04349	-0.13
60.00	454.7	0.02592	0.00	140.00	1571.0	0.12728	-0.02	130.00	436.0	0.01982	-0.05	250.00	1084.0	0.07817	-0.03
60.00	904.9	0.05231	0.12	150.00	401.0	0.02679	0.09	130.00	910.8	0.04349	0.09	250.00	1282.9	0.10019	0.15
60.00	1322.0	0.07542	-0.24	150.00	630.6	0.04901	-0.08	130.00	1648.0	0.07817	-0.07	250.00	1540.3	0.12996	-0.05
60.00	1693.7	0.09596	0.13	150.00	934.8	0.07759	0.09	130.00	2138.6	0.10019	0.03	250.00	1540.3	0.12996	-0.05
70.00	454.7	0.02592	-0.06	150.00	1239.3	0.10488	-0.04	140.00	428.3	0.01982	0.08	250.00	520.3	0.02590	0.02
70.00	909.8	0.05231	0.11	150.00	1497.2	0.12728	0.00	140.00	879.8	0.04349	-0.10	35.00	1087.0	0.05144	0.07
70.00	1252.5	0.07542	-0.15	160.00	409.6	0.02679	0.05	140.00	1574.3	0.07817	-0.03	35.00	1605.5	0.07382	-0.13
70.00	1606.4	0.09596	0.17	160.00	623.6	0.04901	-0.10	140.00	2037.1	0.10019	0.06	35.00	2346.0	0.10356	0.06
70.00	2043.2	0.11975	-0.08	160.00	906.6	0.07759	0.07	150.00	423.3	0.01982	0.03	50.00	488.4	0.02590	0.06
80.00	421.6	0.02592	0.01	160.00	1188.7	0.10488	-0.01	150.00	1502.8	0.07817	-0.03	50.00	2150.4	0.10365	0.04
80.00	824.2	0.05231	0.10	160.00	1478.0	0.12728	0.00	150.00	2027.7	0.10019	0.04	70.00	440.5	0.02590	-0.04
80.00	1199.7	0.07542	-0.21	160.00	422.1	0.02679	0.04	150.00	421.4	0.01982	0.04	70.00	898.8	0.05144	0.04
80.00	1520.3	0.09596	0.09	170.00	620.3	0.04901	-0.10	160.00	822.5	0.04349	-0.03	70.00	1327.2	0.07382	-0.11
80.00	1923.8	0.11975	0.00	170.00	981.7	0.07759	0.09	160.00	1764.3	0.10019	0.03	70.00	1927.9	0.10356	0.01
90.00	419.5	0.02592	-0.02	170.00	1142.0	0.10488	-0.02	160.00	1438.3	0.07817	-0.03	70.00	2429.1	0.12677	0.01
90.00	791.2	0.05231	0.10	170.00	1362.1	0.12728	0.00	160.00	1847.2	0.10019	0.04	70.00	363.8	0.02590	0.10
90.00	1133.2	0.07542	-0.18	180.00	420.4	0.02679	0.06	170.00	423.3	0.01982	-0.03	110.00	741.1	0.05144	0.00
90.00	1442.5	0.09596	0.12	180.00	638.1	0.04901	-0.14	170.00	800.8	0.04349	0.02	110.00	1090.9	0.07382	-0.17
90.00	1819.9	0.11975	-0.07	180.00	958.8	0.07759	0.07	170.00	1380.3	0.07817	0.02	110.00	1578.9	0.10356	0.01
100.00	415.1	0.02592	0.03	180.00	1054.8	0.10488	-0.02	180.00	1697.5	0.12996	-0.07	140.00	1375.0	0.10356	0.03
100.00	763.2	0.05231	0.13	180.00	1298.3	0.12728	0.01	180.00	2198.2	0.12996	0.02	140.00	1725.9	0.12677	0.03
100.00	1092.6	0.07542	-0.17	190.00	428.3	0.02679	0.08	180.00	428.3	0.01982	0.01	140.00	2057.6	0.14764	0.01
100.00	1371.5	0.09596	0.07	190.00	623.7	0.04901	-0.14	180.00	783.4	0.04349	-0.06	140.00	281.2	0.02590	-0.10
100.00	1722.0	0.11975	-0.00	190.00	840.4	0.07759	0.07	180.00	1280.7	0.07817	-0.05	160.00	597.9	0.05144	0.05
110.00	415.1	0.02592	0.01	190.00	1054.8	0.10488	-0.02	180.00	1326.7	0.10019	0.01	160.00	874.5	0.07382	-0.15
110.00	740.2	0.05231	0.09	200.00	481.5	0.02679	0.04	190.00	459.0	0.01982	0.04	160.00	1258.3	0.10356	0.06
110.00	1038.0	0.07542	-0.18	200.00	628.9	0.04901	-0.08	200.00	761.7	0.04349	-0.08	160.00	1571.4	0.12677	0.01
110.00	1306.4	0.09596	0.12	200.00	821.2	0.07759	0.05	200.00	1238.2	0.07817	-0.05	160.00	1877.9	0.14764	0.01
110.00	1633.2	0.11975	-0.07	200.00	1010.3	0.10488	-0.05	190.00	1617.5	0.12996	-0.05	180.00	281.2	0.02590	-0.10
120.00	419.1	0.02592	0.02	200.00	1168.0	0.12728	0.11	190.00	2092.7	0.12996	0.03	180.00	597.9	0.05144	0.05
120.00	721.8	0.05231	0.30	200.00	1298.3	0.12728	0.01	190.00	2092.7	0.12996	0.03	180.00	874.5	0.07382	-0.15
120.00	998.8	0.07542	0.03	210.00	481.5	0.02679	0.04	200.00	549.0	0.01982	0.04	180.00	1155.0	0.10356	0.05
120.00	1248.5	0.09596	0.38	210.00	507.8	0.02679	0.11	200.00	761.7	0.04349	-0.08	180.00	1444.5	0.12677	0.00
120.00	1549.7	0.11975	0.54	210.00	635.1	0.04901	-0.20	200.00	1038.2	0.07817	-0.06	180.00	1716.5	0.14764	0.01
130.00	427.0	0.02592	0.06	210.00	798.2	0.07759	0.13	200.00	1238.2	0.07817	-0.05	180.00	281.2	0.02590	-0.10
130.00	708.7	0.05231	0.04	210.00	958.0	0.10488	-0.09	200.00	1550.9	0.10019	0.15	180.00	597.9	0.05144	0.05
130.00	965.5	0.07542	-0.21	210.00	1089.3	0.12728	0.04	200.00	1996.7	0.12996	-0.05	180.00	874.5	0.07382	-0.17
130.00	1192.3	0.09596	0.04	210.00	1234.2	0.12728	0.02	210.00	459.2	0.01931	0.09	180.00	1155.0	0.10356	0.05
130.00	1476.0	0.11975	0.07	210.00	1463.0	0.14764	0.04	210.00	655.5	0.04349	-0.08	180.00	1444.5	0.12677	0.00
140.00	440.2	0.02592	-0.01	210.00	1633.0	0.14764	0.06	210.00	1202.3	0.07817	-0.14	200.00	1716.5	0.14764	0.01
140.00	699.3	0.05231	0.09	210.00	1822.5	0.10488	-0.11	210.00	1693.4	0.13019	0.06	200.00	267.8	0.02590	-0.02
140.00	935.1	0.07542	-0.19	210.00	2254.1	0.12728	-0.03	210.00	1908.7	0.12996	0.03	200.00	597.9	0.05144	0.05
140.00	1166.5	0.09596	0.09	210.00	254.1	0.02679	0.07	210.00	459.2	0.01982	0.04	200.00	874.5	0.07382	-0.15
140.00	1401.8	0.11975	0.05	210.00	431.8	0.02679	0.07	210.00	655.5	0.04349	-0.08	200.00	1155.0	0.10356	0.05
150.00	457.4	0.02592	0.05	210.00	507.8	0.02679	0.11	210.00	1038.2	0.07817	-0.06	200.00	1326.9	0.12677	0.01
150.00	694.6	0.05231	0.06	210.00	635.1	0.04901	-0.20	210.00	1238.2	0.07817	-0.05	200.00	1571.4	0.14764	0.01
150.00	909.8	0.07542	-0.21	210.00	798.2	0.07759	0.13	210.00	1550.9	0.10019	0.15	200.00	1716.5	0.14764	0.01
150.00	1192.6	0.09596	0.05	210.00	958.0	0.10488	-0.09	210.00	1996.7	0.12996	-0.05	200.00	281.2	0.02590	-0.10
150.00	1433.9	0.11975	0.06	210.00	1089.3	0.12728	0.04	210.00	2254.1	0.12728	0.02	200.00	597.9	0.05144	0.05
150.00	1621.7	0.14764	0.04	210.00	1234.2	0.12728	0.02	210.00	254.1						

TABLE III. CONTINUED

n-DECANE (CONTINUED)				1,4-DIMETHYLBENZENE				1-METHYLMETHYLENE			
°C	psi	α_2	ΔZ	°C	psi	α_2	ΔZ	°C	psi	α_2	ΔZ
240.00	258.7	0.02590	0.01	180.00	502.8	0.02521	0.03	210.00	431.4	0.02808	-0.11
240.00	462.1	0.05144	0.08	180.00	1573.0	0.07906	-0.11	210.00	772.7	0.05078	0.18
240.00	649.5	0.07382	-0.11	180.00	2083.4	0.10211	-0.06	210.00	1168.0	0.07567	0.06
240.00	908.7	0.10356	-0.02	200.00	932.1	0.05130	0.02	210.00	2045.6	0.12688	-0.24
240.00	1222.3	0.12677	-0.01	200.00	1440.4	0.07906	-0.04	220.00	419.3	0.02808	-0.05
240.00	1322.3	0.14764	-0.02	200.00	1982.7	0.10211	-0.02	220.00	745.7	0.05078	0.16
250.00	1672.5	0.02590	0.03	200.00	2425.9	0.12907	-0.07	220.00	1123.1	0.07567	0.04
250.00	260.5	0.05144	-0.06	210.00	895.5	0.05130	0.03	220.00	1515.1	0.10000	-0.30
250.00	453.2	0.07382	-0.12	210.00	1390.5	0.07906	-0.05	230.00	1958.6	0.12688	-0.17
250.00	630.5	0.10356	-0.01	220.00	1902.5	0.10211	-0.03	230.00	2720.9	0.15078	0.04
250.00	875.7	0.13566	-0.09	220.00	2400.0	0.12677	-0.05	240.00	409.2	0.02808	-0.04
250.00	1077.6	0.16777	-0.02	220.00	3126.5	0.14906	-0.05	240.00	720.9	0.05078	0.11
250.00	1266.1	0.19764	-0.05	220.00	3852.0	0.17130	-0.03	240.00	1080.3	0.07567	0.05
250.00	1454.6	0.22750	-0.03	220.00	4577.5	0.19357	-0.04	240.00	1453.6	0.10000	-0.30
250.00	1643.1	0.25736	-0.04	220.00	5303.0	0.21584	-0.03	240.00	1875.9	0.12688	-0.16
250.00	1831.6	0.28722	-0.02	220.00	6028.5	0.23811	-0.01	240.00	2300.0	0.15078	0.06
250.00	2020.1	0.31708	-0.01	220.00	6754.0	0.26038	-0.02	240.00	2720.9	0.17468	-0.07
250.00	2208.6	0.34694	-0.01	220.00	7479.5	0.28265	-0.01	240.00	3140.8	0.19858	-0.04
250.00	2397.1	0.37680	-0.01	220.00	8205.0	0.30492	-0.01	240.00	3560.7	0.22222	0.05
250.00	2585.6	0.40666	-0.01	220.00	8930.5	0.32719	-0.01	240.00	3980.6	0.24688	-0.07
250.00	2774.1	0.43652	-0.01	220.00	9656.0	0.34946	-0.01	240.00	4400.5	0.27088	-0.09
250.00	2962.6	0.46638	-0.01	220.00	10381.5	0.37173	-0.01	240.00	4820.4	0.29488	-0.11
250.00	3151.1	0.49624	-0.01	220.00	11107.0	0.39400	-0.01	240.00	5240.3	0.31888	-0.13
250.00	3339.6	0.52610	-0.01	220.00	11832.5	0.41627	-0.01	240.00	5660.2	0.34288	-0.15
250.00	3528.1	0.55596	-0.01	220.00	12558.0	0.43854	-0.01	240.00	6080.1	0.36688	-0.17
250.00	3716.6	0.58582	-0.01	220.00	13283.5	0.46081	-0.01	240.00	6500.0	0.39088	-0.19
250.00	3905.1	0.61568	-0.01	220.00	14009.0	0.48308	-0.01	240.00	6920.0	0.41488	-0.21
250.00	4093.6	0.64554	-0.01	220.00	14734.5	0.50535	-0.01	240.00	7340.0	0.43888	-0.23
250.00	4282.1	0.67540	-0.01	220.00	15460.0	0.52762	-0.01	240.00	7760.0	0.46288	-0.25
250.00	4470.6	0.70526	-0.01	220.00	16185.5	0.54989	-0.01	240.00	8180.0	0.48688	-0.27
250.00	4659.1	0.73512	-0.01	220.00	16911.0	0.57216	-0.01	240.00	8600.0	0.51088	-0.29
250.00	4847.6	0.76498	-0.01	220.00	17636.5	0.59443	-0.01	240.00	9020.0	0.53488	-0.31
250.00	5036.1	0.79484	-0.01	220.00	18362.0	0.61670	-0.01	240.00	9440.0	0.55888	-0.33
250.00	5224.6	0.82470	-0.01	220.00	19087.5	0.63897	-0.01	240.00	9860.0	0.58288	-0.35
250.00	5413.1	0.85456	-0.01	220.00	19813.0	0.66124	-0.01	240.00	10280.0	0.60688	-0.37
250.00	5601.6	0.88442	-0.01	220.00	20538.5	0.68351	-0.01	240.00	10700.0	0.63088	-0.39
250.00	5790.1	0.91428	-0.01	220.00	21264.0	0.70578	-0.01	240.00	11120.0	0.65488	-0.41
250.00	5978.6	0.94414	-0.01	220.00	21989.5	0.72805	-0.01	240.00	11540.0	0.67888	-0.43
250.00	6167.1	0.97400	-0.01	220.00	22715.0	0.75032	-0.01	240.00	11960.0	0.70288	-0.45
250.00	6355.6	0.10000	-0.01	220.00	23440.5	0.77259	-0.01	240.00	12380.0	0.72688	-0.47
250.00	6544.1	0.10000	-0.01	220.00	24166.0	0.79486	-0.01	240.00	12800.0	0.75088	-0.49
250.00	6732.6	0.10000	-0.01	220.00	24891.5	0.81713	-0.01	240.00	13220.0	0.77488	-0.51
250.00	6921.1	0.10000	-0.01	220.00	25617.0	0.83940	-0.01	240.00	13640.0	0.79888	-0.53
250.00	7109.6	0.10000	-0.01	220.00	26342.5	0.86167	-0.01	240.00	14060.0	0.82288	-0.55
250.00	7298.1	0.10000	-0.01	220.00	27068.0	0.88394	-0.01	240.00	14480.0	0.84688	-0.57
250.00	7486.6	0.10000	-0.01	220.00	27793.5	0.90621	-0.01	240.00	14900.0	0.87088	-0.59
250.00	7675.1	0.10000	-0.01	220.00	28519.0	0.92848	-0.01	240.00	15320.0	0.89488	-0.61
250.00	7863.6	0.10000	-0.01	220.00	29244.5	0.95075	-0.01	240.00	15740.0	0.91888	-0.63
250.00	8052.1	0.10000	-0.01	220.00	29970.0	0.97302	-0.01	240.00	16160.0	0.94288	-0.65
250.00	8240.6	0.10000	-0.01	220.00	30695.5	0.99529	-0.01	240.00	16580.0	0.96688	-0.67
250.00	8429.1	0.10000	-0.01	220.00	31421.0	1.01756	-0.01	240.00	17000.0	0.99088	-0.69
250.00	8617.6	0.10000	-0.01	220.00	32146.5	1.03983	-0.01	240.00	17420.0	1.01488	-0.71
250.00	8806.1	0.10000	-0.01	220.00	32872.0	1.06210	-0.01	240.00	17840.0	1.03888	-0.73
250.00	8994.6	0.10000	-0.01	220.00	33597.5	1.08437	-0.01	240.00	18260.0	1.06288	-0.75
250.00	9183.1	0.10000	-0.01	220.00	34323.0	1.10664	-0.01	240.00	18680.0	1.08688	-0.77
250.00	9371.6	0.10000	-0.01	220.00	35048.5	1.12891	-0.01	240.00	19100.0	1.11088	-0.79
250.00	9560.1	0.10000	-0.01	220.00	35774.0	1.15118	-0.01	240.00	19520.0	1.13488	-0.81
250.00	9748.6	0.10000	-0.01	220.00	36500.0	1.17345	-0.01	240.00	19940.0	1.15888	-0.83
250.00	9937.1	0.10000	-0.01	220.00	37225.5	1.19572	-0.01	240.00	20360.0	1.18288	-0.85
250.00	10125.6	0.10000	-0.01	220.00	37951.0	1.21799	-0.01	240.00	20780.0	1.20688	-0.87
250.00	10314.1	0.10000	-0.01	220.00	38676.5	1.24026	-0.01	240.00	21200.0	1.23088	-0.89
250.00	10502.6	0.10000	-0.01	220.00	39402.0	1.26253	-0.01	240.00	21620.0	1.25488	-0.91
250.00	10691.1	0.10000	-0.01	220.00	40127.5	1.28480	-0.01	240.00	22040.0	1.27888	-0.93
250.00	10879.6	0.10000	-0.01	220.00	40853.0	1.30707	-0.01	240.00	22460.0	1.30288	-0.95
250.00	11068.1	0.10000	-0.01	220.00	41578.5	1.32934	-0.01	240.00	22880.0	1.32688	-0.97
250.00	11256.6	0.10000	-0.01	220.00	42304.0	1.35161	-0.01	240.00	23300.0	1.35088	-0.99
250.00	11445.1	0.10000	-0.01	220.00	43029.5	1.37388	-0.01	240.00	23720.0	1.37488	-1.01
250.00	11633.6	0.10000	-0.01	220.00	43755.0	1.39615	-0.01	240.00	24140.0	1.39888	-1.03
250.00	11822.1	0.10000	-0.01	220.00	44480.5	1.41842	-0.01	240.00	24560.0	1.42288	-1.05
250.00	12010.6	0.10000	-0.01	220.00	45206.0	1.44069	-0.01	240.00	24980.0	1.44688	-1.07
250.00	12199.1	0.10000	-0.01	220.00	45931.5	1.46296	-0.01	240.00	25400.0	1.47088	-1.09
250.00	12387.6	0.10000	-0.01	220.00	46657.0	1.48523	-0.01	240.00	25820.0	1.49488	-1.11
250.00	12576.1	0.10000	-0.01	220.00	47382.5	1.50750	-0.01	240.00	26240.0	1.51888	-1.13
250.00	12764.6	0.10000	-0.01	220.00	48108.0	1.52977	-0.01	240.00	26660.0	1.54288	-1.15
250.00	12953.1	0.10000	-0.01	220.00	48833.5	1.55204	-0.01	240.00	27080.0	1.56688	-1.17
250.00	13141.6	0.10000	-0.01	220.00	49559.0	1.57431	-0.01	240.00	27500.0	1.59088	-1.19
250.00	13330.1	0.10000	-0.01	220.00	50284.5	1.59658	-0.01	240.00	27920.0	1.61488	-1.21
250.00	13518.6	0.10000	-0.01	220.00	51010.0	1.61885	-0.01	240.00	28340.0	1.63888	-1.23
250.00	13707.1	0.10000	-0.01	220.00	51735.5	1.64112	-0.01	240.00	28760.0	1.66288	-1.25
250.00	13895.6	0.10000	-0.01	220.00	52461.0	1.66339	-0.01	240.00	29180.0	1.68688	-1.27
250.00	14084.1	0.10000	-0.01	220.00	53186.5	1.68566	-0.01	240.00	29600.0	1.71088	-1.29
250.00	14272.6	0.10000	-0.01	220.00	53912.0	1.70793	-0.01	240.00	30020.0	1.73488	-1.31
250.00	14461.1	0.10000	-0.01	220.00	54637.5	1.73020	-0.01	240.00	30440.0	1.75888	-1.33
250.00	14649.6	0.10000	-0.01	220.00	55363.0	1.75247	-0.01	240.00	30860.0	1.78288	-1.35
250.00	14838.1	0.10000	-0.01	220.00	56088.5	1.77474	-0.01	240.00	31280.0	1.80688	-1.37
250.00	15026.6	0.10000	-0.01	220.00	56814.0	1.79701	-0.01	240.00	31700.0	1.83088	-1.39
250.00	15215.1	0.10000	-0.01	220.00	57539.5	1.81928	-0.01	240.00	32120.0	1.85488	-1.41
250.00	15403.6	0.10000	-0.01	220.00	58265.0	1.84155	-0.01	240.00	32540.0	1.87888	-1.43
250.00	15592.1	0.10000	-0.01	220.00	58990.5	1.86382	-0.01	240.00	32960.0	1.9	

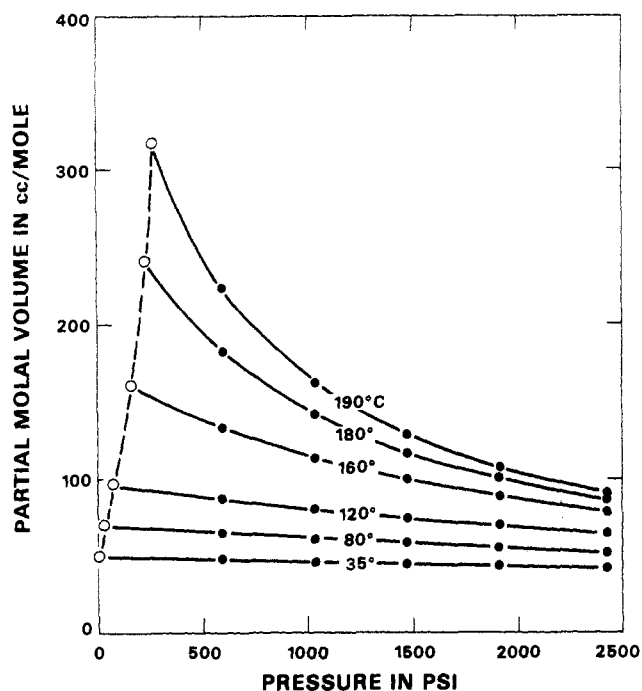


Figure 10. Partial molal volumes of hydrogen, at infinite dilution, in liquid 2,3-dimethylbutane.

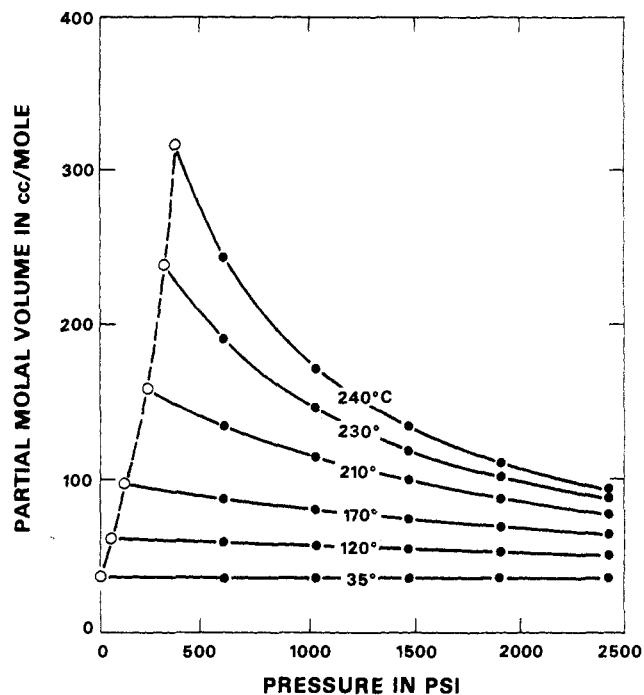


Figure 12. Partial molal volumes of hydrogen, at infinite dilution, in liquid cyclohexane.

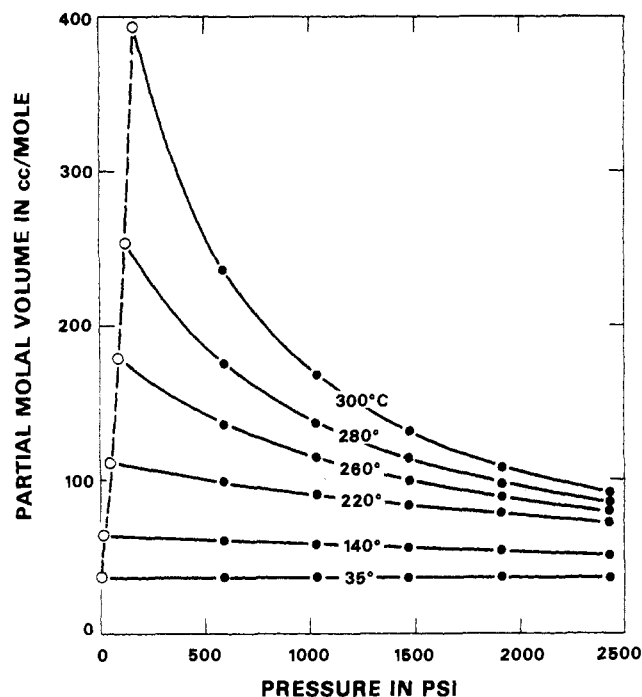


Figure 11. Partial molal volumes of hydrogen, at infinite dilution, in liquid *n*-decane.

pressure variation of c' is taken care of, between p_1^0 and 2500 psi, by a single term in reciprocal pressure. Thus, eq 3 may be rewritten as

$$\Delta V/n_2 = 100/(a + bu - cu^2) + 100dx_2/u \quad (8)$$

where $u = \text{atmospheres}/100 = \text{psi}/1469.6$, and a , b , c , and d are functions of temperature only.

A nonlinear regression program was used to fit eq 8 to each experimental set of $\Delta V/n_2$ in the supplementary material tables which corresponded to a system at a particular temperature (usually about 30 points). To obtain best values for \bar{V}_2^* a two-step procedure was used. With $c = 0$, eq 8 was fitted by using only values of $\Delta V/n_2$ in the linear region (below 1600

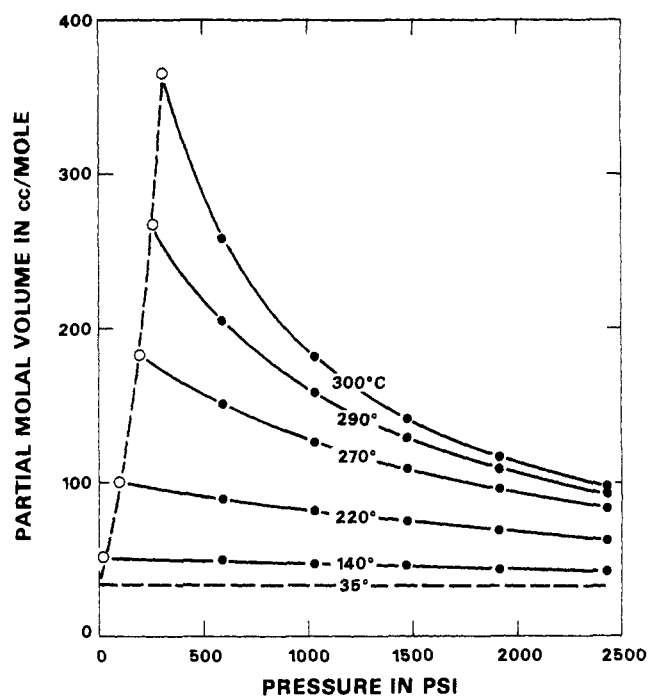


Figure 13. Partial molal volumes of hydrogen, at infinite dilution, in liquid *m*-xylene.

psi). Then a second fit was made by using the complete eq 8 with a , b , and d fixed at the values derived in the first fit, and with no restriction on pressure. a , b , and d , as derived in the first fit, and c , as derived in the second fit, are listed in Table VI. Deviations listed in Table VI and in the supplementary material refer to the second fit.

Partial molal volumes of hydrogen at infinite dilution in hydrocarbons, \bar{V}_2^* , were calculated from constants of Table VI and plotted in Figures 9-14. The nearly vertical dashed lines represent vapor pressures of the pure hydrocarbons. Some lower pressure points are shown as open circles to indicate that they are the result of a double linear extrapolation, i.e., into regions of both composition and pressure which are below

Table VI. Liquid Volume Dilations on Mixing Hydrogen and Hydrocarbons^a

°C	n-pentane				2,3 dimethyl butane				cyclohexane				n-decane				m-xylene				1,4-difethyl benzene				
	a	b	c	d	a	b	c	d	a	b	c	d	a	b	c	d	a	b	c	d	a	b	c	d	
35	1.88	.27			1.4	2.02	.22		1.2	2.74			2.4	2.73							2.91				2.3
40	1.58	.39			3.5	2.12	.14		1.3												2.86				1.3
50	1.61	.32			3.6	1.88	.20		1.3	2.54			2.5								2.69				1.2
60	1.41	.37			3.5	1.79	.19		2.3	2.31	.29		3.5								2.86				1.4
70	1.35	.32			2.4	1.54	.30		1.3	2.25	.18		2.5								2.71				2.3
80	1.20	.34			3.6	1.42	.31		2.4	1.84	.26		2.5								2.63				2.4
90	1.14	.31			3.6	1.36	.25		2.3	1.93	.20		2.4								2.51				2.3
100	1.02	.35			2.4	1.29	.27		2.4	1.76	.31		3.6												2.3
110	.88	.37			2.4	1.17	.30		3.5	1.63	.25		2.5	1.95	.18		2.4								2.3
120	.75	.39			2.7	1.02	.31		2.5	1.61	.21		2.4												2.3
130	.62	.42			3.5	.90	.32		2.5	1.56	.13		1.3												2.3
140	.57	.47			1.3	2.6	.78	.38	.5	3.7	1.35	.21	2.6	1.56	.23		2.5	1.95	.24						2.3
150	.40	.56	.03		1.6	2.5	.67	.42	.8	3.6	1.25	.23	2.4												2.6
160	.24	.64	.04		2.0	3.6	.58	.44	1.0	3.6	1.12	.30	3.6	1.29	.24		2.3	1.56	.27						2.6
170					.45	.43			1.0	3.6	1.01	.33	.8	1.3											2.6
180					.33	.56	.04		1.9	3.6	.93	.32	.9	2.5	1.27	.25	.6	2.4	1.44	.23					2.4
190					.20	.62	.05		2.4	3.7	.77	.37	.9	2.6											2.4
200					.69	.36			1.1	3.8	1.10	.32	1.0	2.6	1.27	.26	1.0	2.6	1.27	.26					2.4
210					.56	.44			2.1	2.4			.7	2.4											2.3
220					.42	.54	.04		2.4	2.6	.89	.30	.7	2.4	.98	.36	1.3	1.3	1.13	.25					2.3
230					.30	.58	.04		3.0	2.6															2.5
240					.17	.63	.05		3.6	3.9	.82	.33	1.5	2.6	.82	.30	1.5	2.6	.82	.30					2.5
250					.63	.37			1.2	2.7	.72	.32	1.2	2.7	.72	.32	1.3	1.5	.97	.29					2.4
260					.53	.53	.05		2.0	2.6	.60	.39	1.8	2.4	.84	.29	1.8	2.4	.84	.29					2.5
270					.42	.53	.06		1.7	2.8	.49	.43	2.2	2.8	.81	.31	2.2	2.8	.81	.31					2.5
280					.35	.58	.05		2.5	3.7	.36	.49	.04	2.2	3.7	.70	.35	1.6	2.5						2.5
290					.26	.61	.06		2.8	4.10	.28	.52	.03	3.1	2.5	.60	.35	1.5	2.5						2.5
300					.18	.61	.03		3.2	3.9	.15	.60	.04	3.9	3.5	.51	.41	2.2	2.6						2.6

^a a, b, c, and d are parameters in eq 8. SD and MD are standard and maximum deviations.

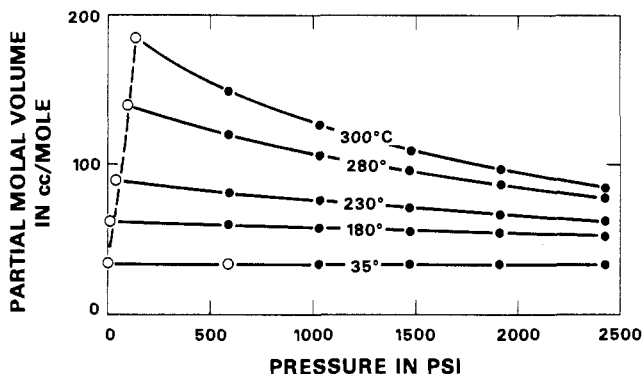


Figure 14. Partial molal volumes of hydrogen, at infinite dilution, in liquid 1,4-diethylbenzene.

those covered by experimental data. The filled-in circles involve only linear extrapolations to $x_2 = 0$, at a constant pressure, within the pressure range of the measurements. Surprisingly, at the lower pressures and higher temperatures, the partial

molal volumes of hydrogen are often larger than those of hydrocarbons.

Registry No. Hydrogen, 1333-74-0; *n*-pentane, 109-66-0; 2,3-dimethylbutane, 79-29-8; cyclohexane, 110-82-7; *n*-decane, 124-18-5; *m*-xylene, 108-38-3; 1,4-diethylbenzene, 105-05-5; 1-methylnaphthylene, 90-12-0.

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Solidification Behavior of the Cinnamic Acid-*p*-Nitrophenol Eutectic System

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The solid-liquid equilibrium of the cinnamic acid-*p*-nitrophenol (CA-*p*NP) eutectic system has been investigated. Heat of fusion, microstructure, and strength measurements have been made. Infrared spectral studies indicate molecular association in the formation of the eutectic. Thermodynamic functions such as h^E , g^E , and S^E have been calculated and were found to be negative except g^E . Statistical mechanical treatment shows that the surface nucleation theory holds good in the solidification of the present eutectic.

Introduction

Solid materials are of considerable interest both from the fundamental and from the technological point of view. Eutectic materials also come in this category. In order to control the properties of such materials, studies of phase diagram, linear velocity of crystallization, microstructure, compressive strength, and thermodynamic properties are essential (1). The present paper describes the chemistry of the cinnamic acid-*p*-nitrophenol (CA-*p*NP) eutectic system with reference to the above properties.

Experimental Section

Materials and Purification. *p*-Nitrophenol (BDH) and cinnamic acid (BDH) were purified by repeated distillation under reduced pressure. The purity was checked by determining the melting points with the help of a mercury thermometer correct to ± 0.1 °C. The melting points are 112.0 and 133.0 °C, respectively. Cinnamic acid is represented as CA and *p*-nitrophenol is represented as *p*NP.

Phase Diagram and Undercooling Study. The phase diagram of the CA-*p*NP system has been studied by the thaw melt method (2). Mixtures of various compositions were prepared

in glass test tubes by repeated heating, chilling, and grinding in a glass mortar. The melting points and thaw points were determined with a mercury thermometer correct to ± 0.1 °C. The undercooling study was made in a manner described by Rastogi and Bassi (3).

Study of Microstructures. A microscopic method was used for the study of microstructures of components and eutectic. A glass slide was kept in an oven at a temperature higher than the melting points of the eutectic, and a very small amount of the sample was placed on it. As the sample melted completely, the coverslip was glided on it. The slide was allowed to cool and nucleations were started from one side and this was then photographed with a camera under a microscope of desired magnification. The effect of 0.1% 8-hydroxyquinoline and 4-chloroaniline on the microstructure of the eutectic has also been investigated.

Heat of Fusion Measurements. The heats of fusion of the pure components and the eutectic were determined by differential thermal analyzer (Paulik-Paulik-Erdey MOM derivatograph, Hungary) using the method of Vold (4). The heating rate was maintained at 2 °C/min, and the temperature was measured by a Pt-Rh thermocouple. From this method only the relative value of the heat of fusion could be determined.

Compressive Strength Measurements. Compressive strengths of components and eutectic in the form of pellets were determined by an universal testing machine. The pellets were prepared by solidifying the molten materials in glass test tubes of uniform diameter and the surfaces were smoothed by rubbing on emery paper. True stress was obtained by dividing the maximum load applied on the pellet (which was capable of breaking the pellet) by the area of the pellet. For calculating true strain, the total number of divisions on the graph (which indicates the maximum compression) was divided by the magnification (magnification was obtained by dividing chart speed by cross head speed) and the value thus obtained was finally divided by the original length of the pellet.